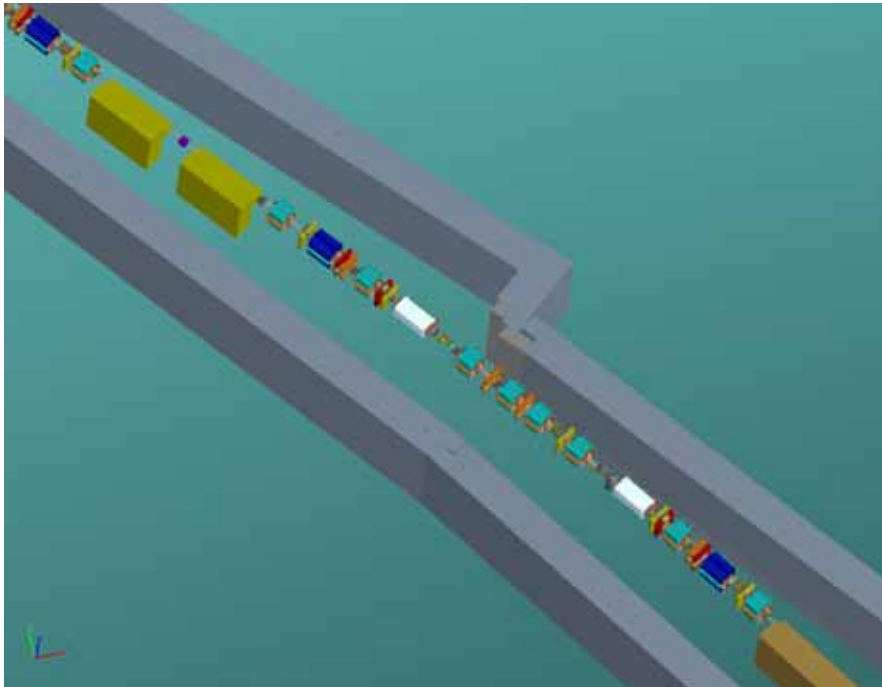


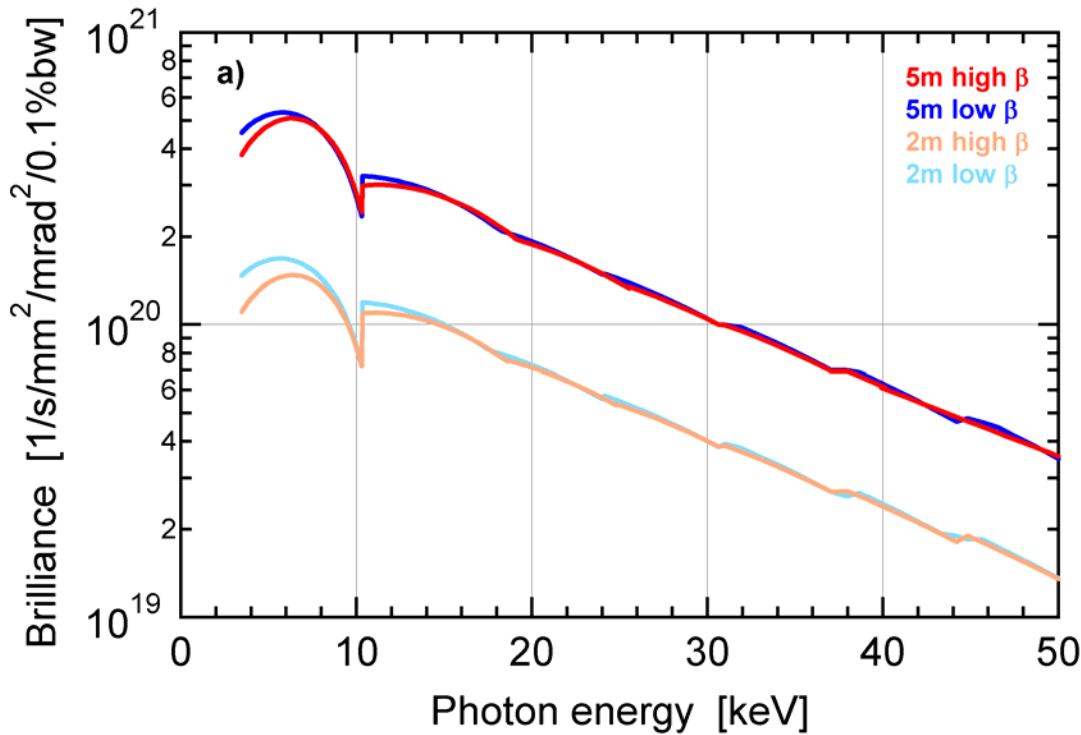


# Insertion Devices for PETRA III

**Markus Tischer, 30.01.06**

- 14 Undulator radiation sources (IDs):
  - 3 IDs for 3 normal straight sections (5m)
  - 10 IDs for 5 canted straight sections (2m)
  - 1 ID for the long straight section (20m)
- **Magnetic design, mechanics, control system for 6 different undulator types:**
  - Conventional IDs (10 St.) :
    - Standard-IDs (2+5m),
    - Spectroscopy-IDs (2m)
  - Special devices (1× each) :
    - High-energy ID (5m),
    - Quasi-periodic ID (2m),
    - Apple2 ID (5m),
    - 20m-ID (4×5m)





Standard ID : (5m length)

- Source size at 10keV  
 $140 \times 5.6 \mu\text{m}^2$ ,  
 $7.9 \times 4.1 \mu\text{rad}^2$
- Power density  
 $0.2 \text{ W}/\mu\text{rad}^2$
- Power in  $1 \times 1 \text{ mm}^2$  (L = 40m)  
 120 W

- **Standard ID**

$K_{\text{max}} := 2.2$  (← tunability demand)

$\lambda_U = 29 \text{ mm}$

$B_0 = 0.81 \text{ T}$

$E_1 = 3450 \text{ eV}$

$P_{\text{tot}} = 7.5 \text{ kW}$  (@ 5m length)

- **Spectroscopy ID**

$K_{\text{max}} = 2.7$

$\lambda_U = 31.4 \text{ mm}$

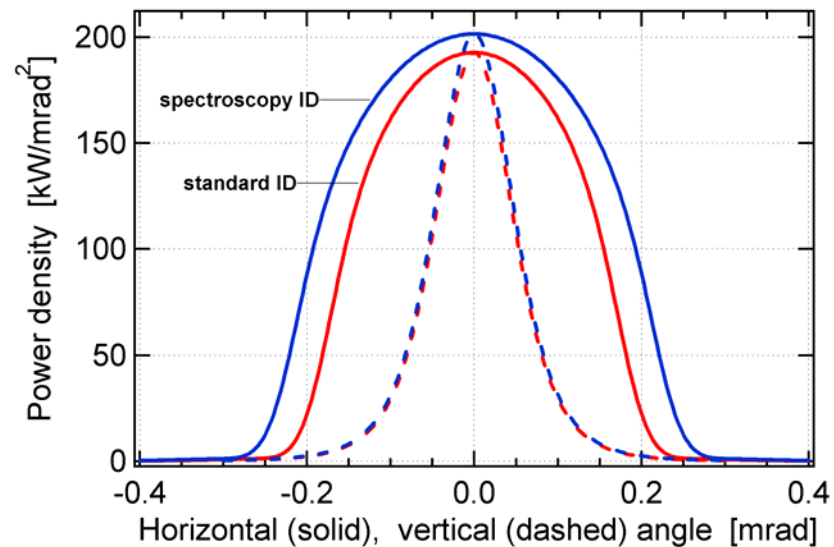
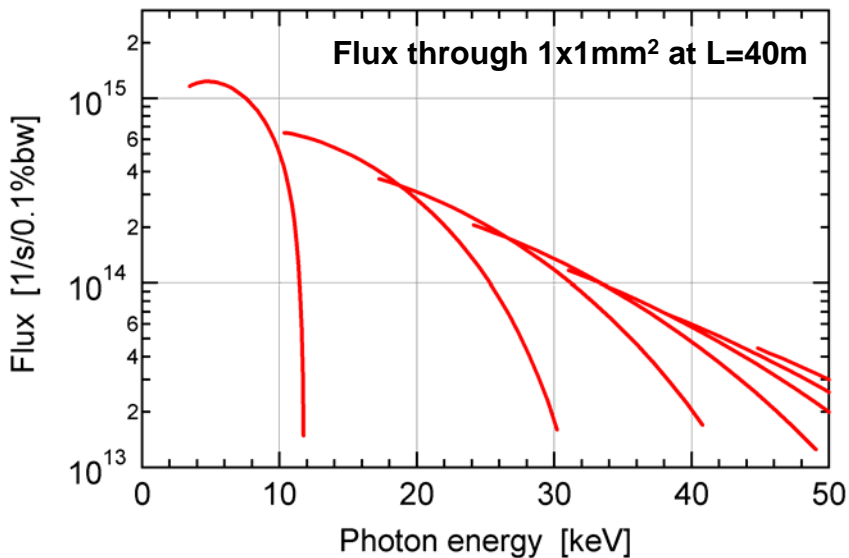
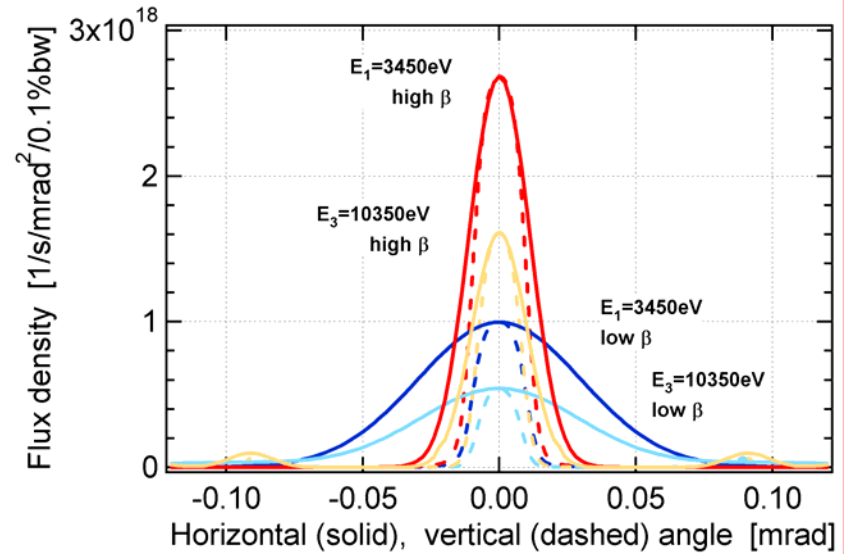
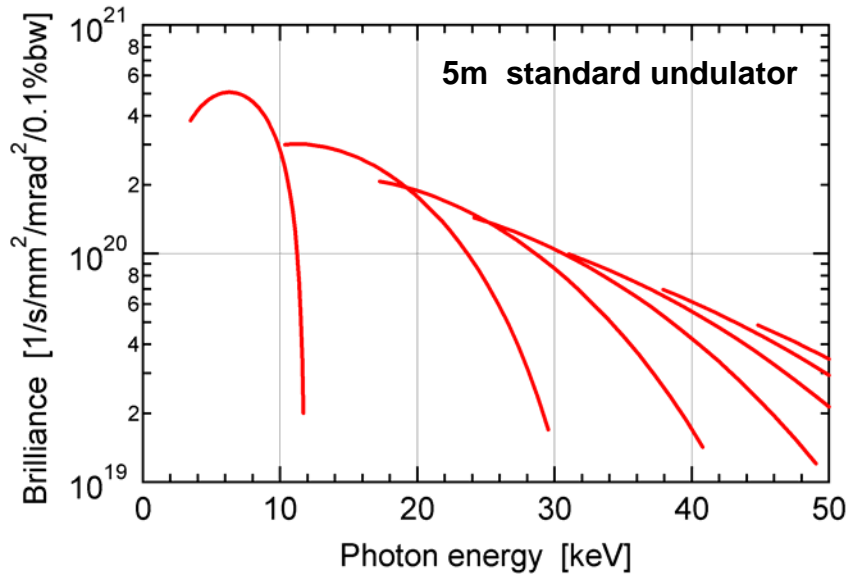
$B_0 = 0.91 \text{ T}$

$E_1 := 2400 \text{ eV}$  (← user demand)

$P_{\text{tot}} = 3.8 \text{ kW}$  (@ 2m length)



# Planar IDs - Properties (2)



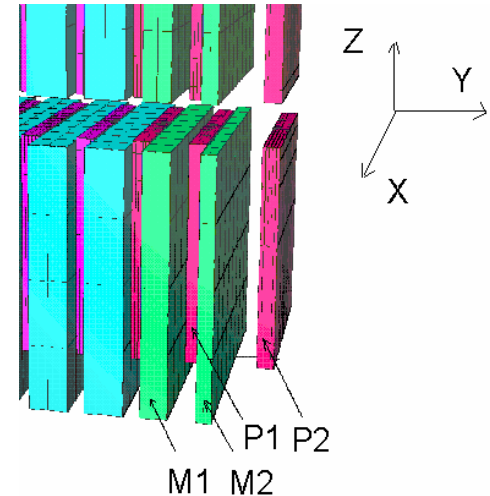
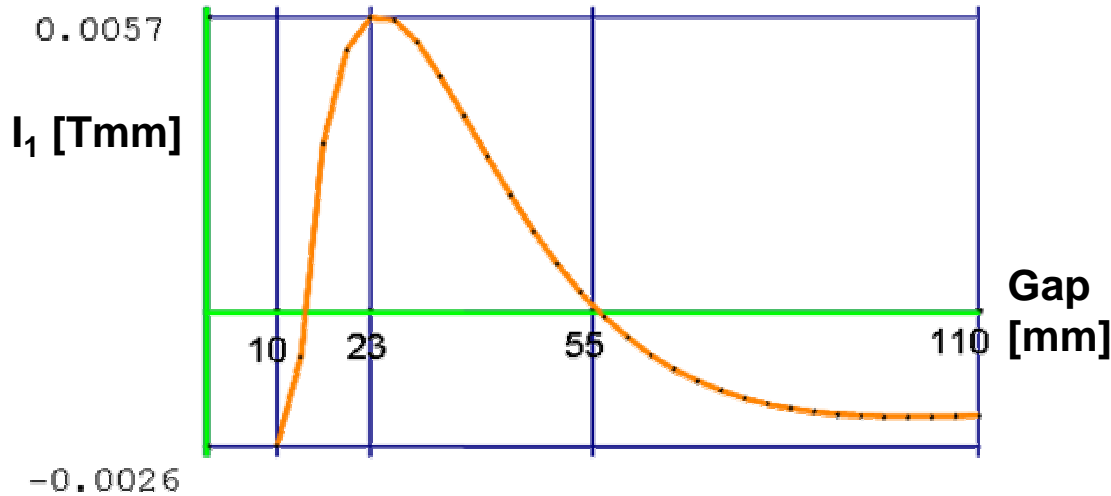
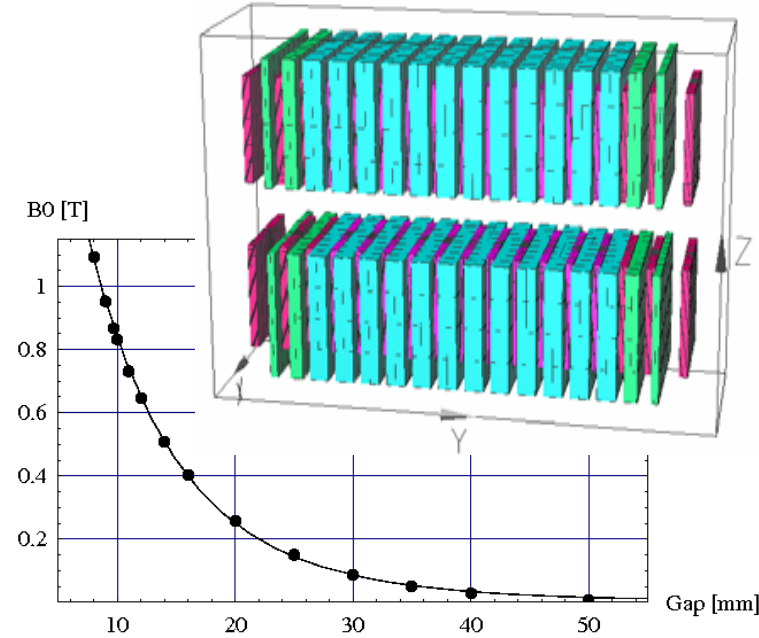


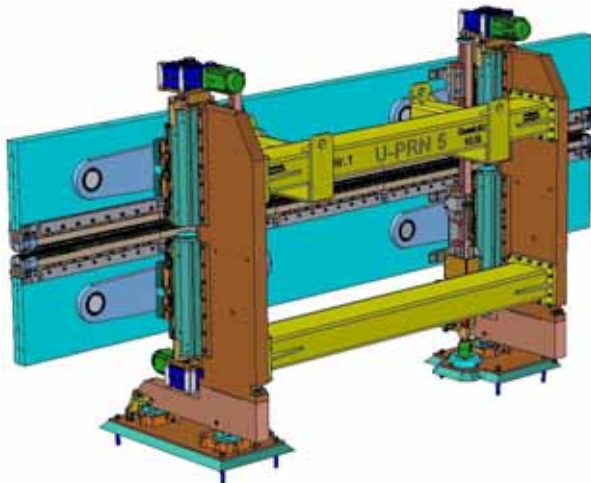
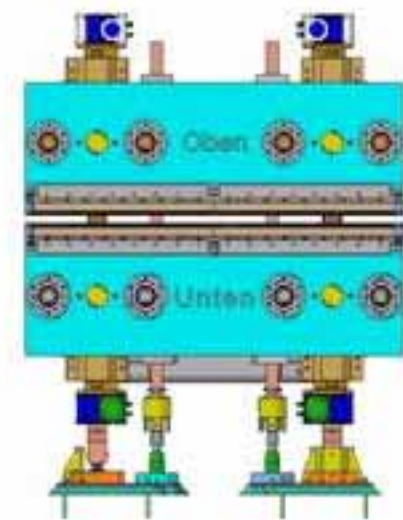
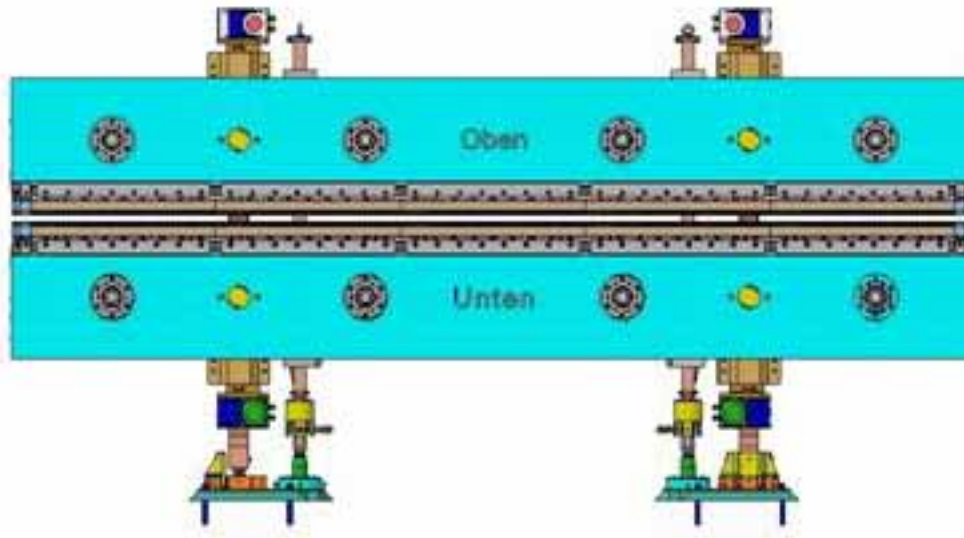
# Development of planar undulators



- **Common Development for PETRA III & XFEL**
  - magnet design & field terminations
  - universal gap mechanics
  - motion control system
  
- **Prototype undulator in the procurement phase**

- Periodic part:**  
 optimize peak field, transverse field roll-off,  
 magnet material, demagnetizing fields
- End structure :**  
 Minimize gap dependence of 1st field integral (kick)  
 realize gap-independent trajectory in the undulator  
 Problem: different iron saturation at center and ends  
 →  $\Delta I_1(\text{gap}) \sim 0.01 \text{Tmm}$  ( $0.5 \mu\text{rad}$ )





- **Requirements**

Minimum girder deformation  $\sim 1\mu\text{m}$

Temperature insensitive

Magnetic forces up to 160kN

Gap accuracy of  $\sim 1\mu\text{m}$

Taper up to 1mm

- **Concept** (ZM1, since Sept.04)

4-fold girder support

Decoupling of guiding and load support

4-axis drive

**XFEL-specifications:**

$$\Delta K/K = 8 \cdot 10^{-5} \Rightarrow$$

Temp. :  $\Delta T = 0.08 \text{ K}$

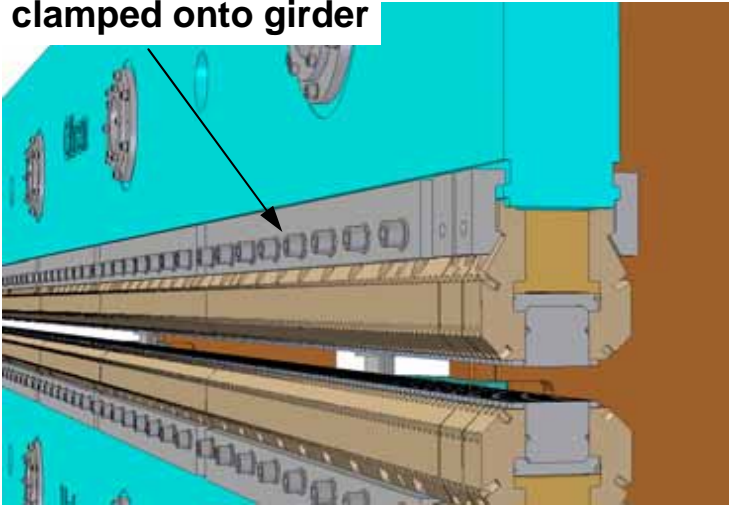
Justage:  $\Delta y = 100 \mu\text{m}$

Taper:  $\Delta g = 1 \mu\text{m}$

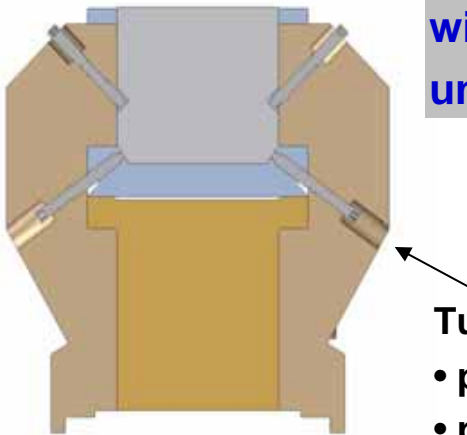
Gap:  $\Delta g = 1 \mu\text{m}$



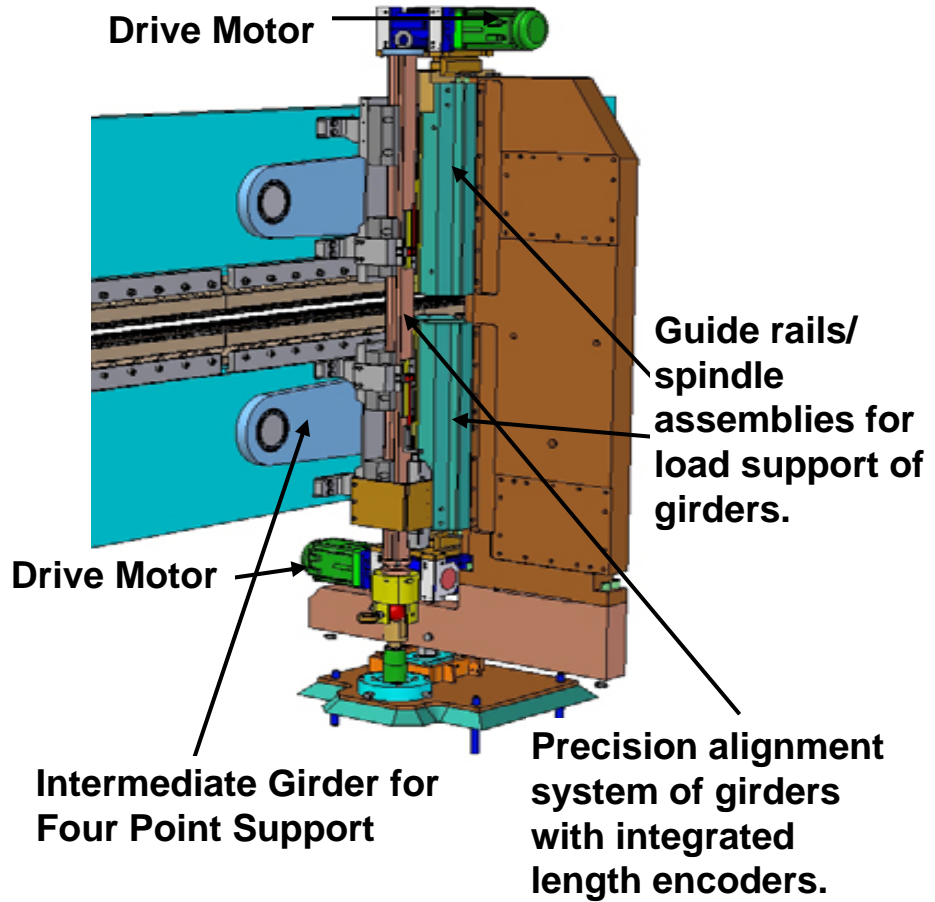
Magnet structure, clamped onto girder



Based on experience with the VUV-FEL undulators



- Tuning of the magnet structure:
- pole height adjustment by  $\pm 0.3\text{mm}$
  - possibly  $\pm 1\text{mrad}$  tilt





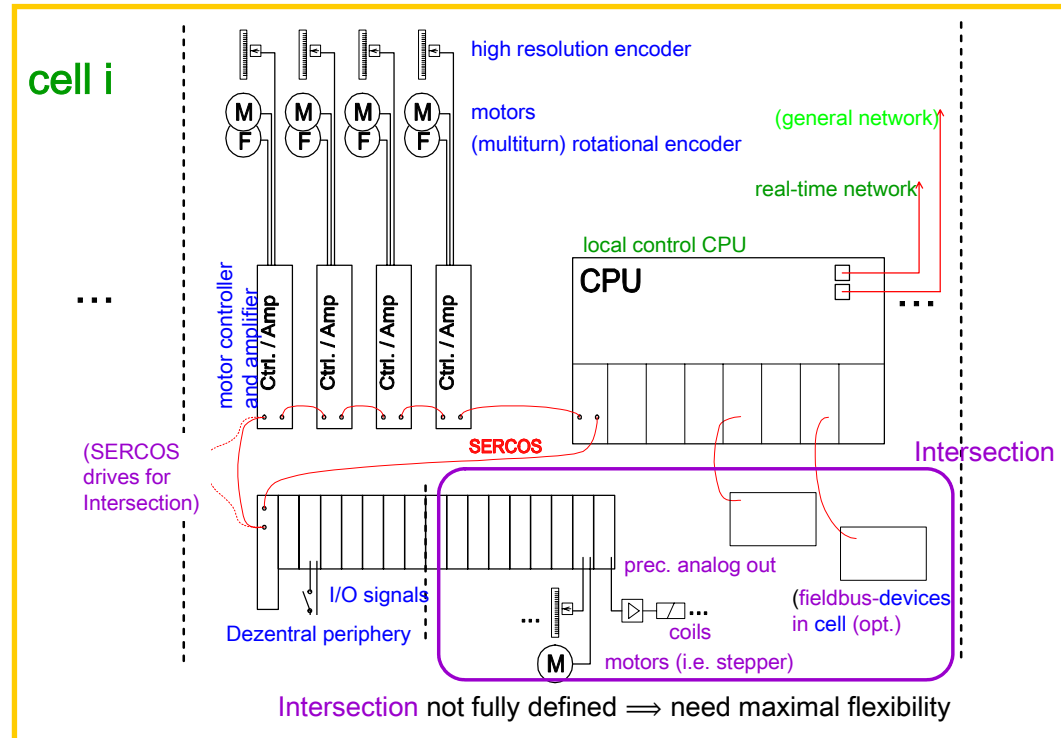


- Requirements & Concept:**
- synchronized gap movements
  - comprise the modular setup => **cells**
  - high reliability
  - allow complex movement-schemes
  - movements with high dynamics
  - long-term availability of components

Experimentally  
proven

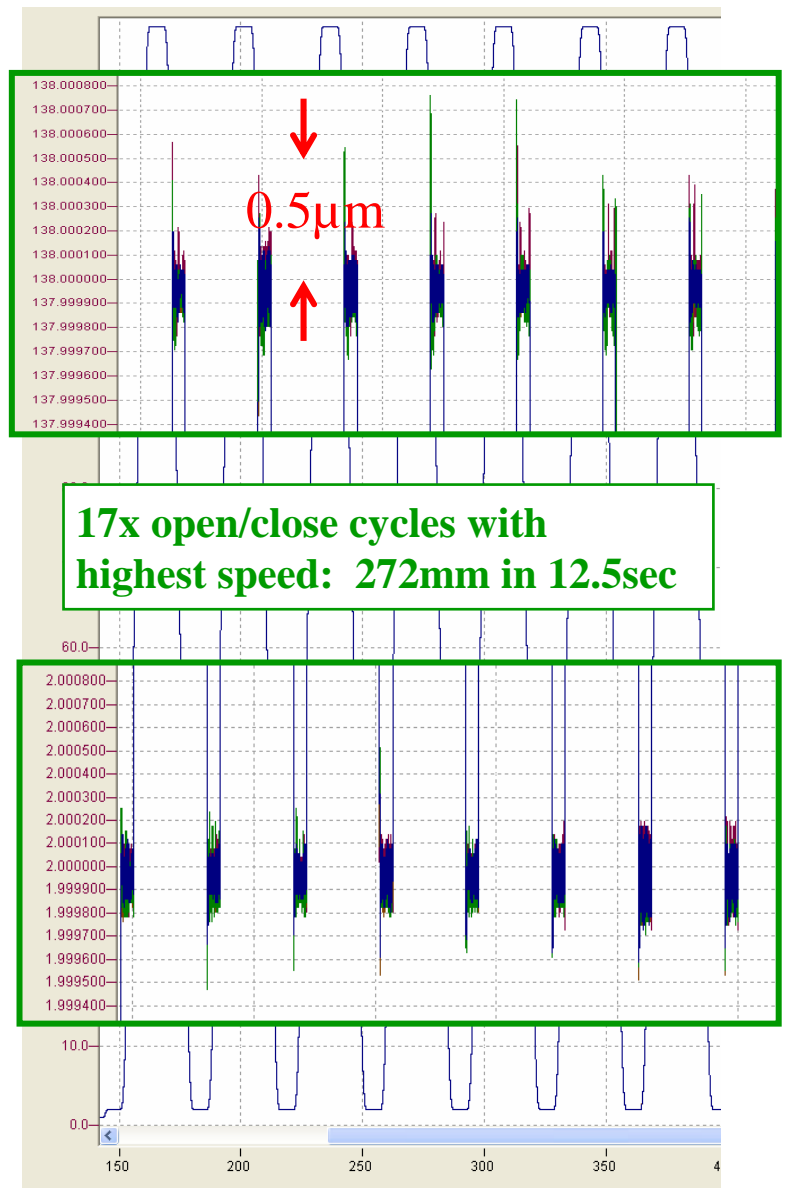
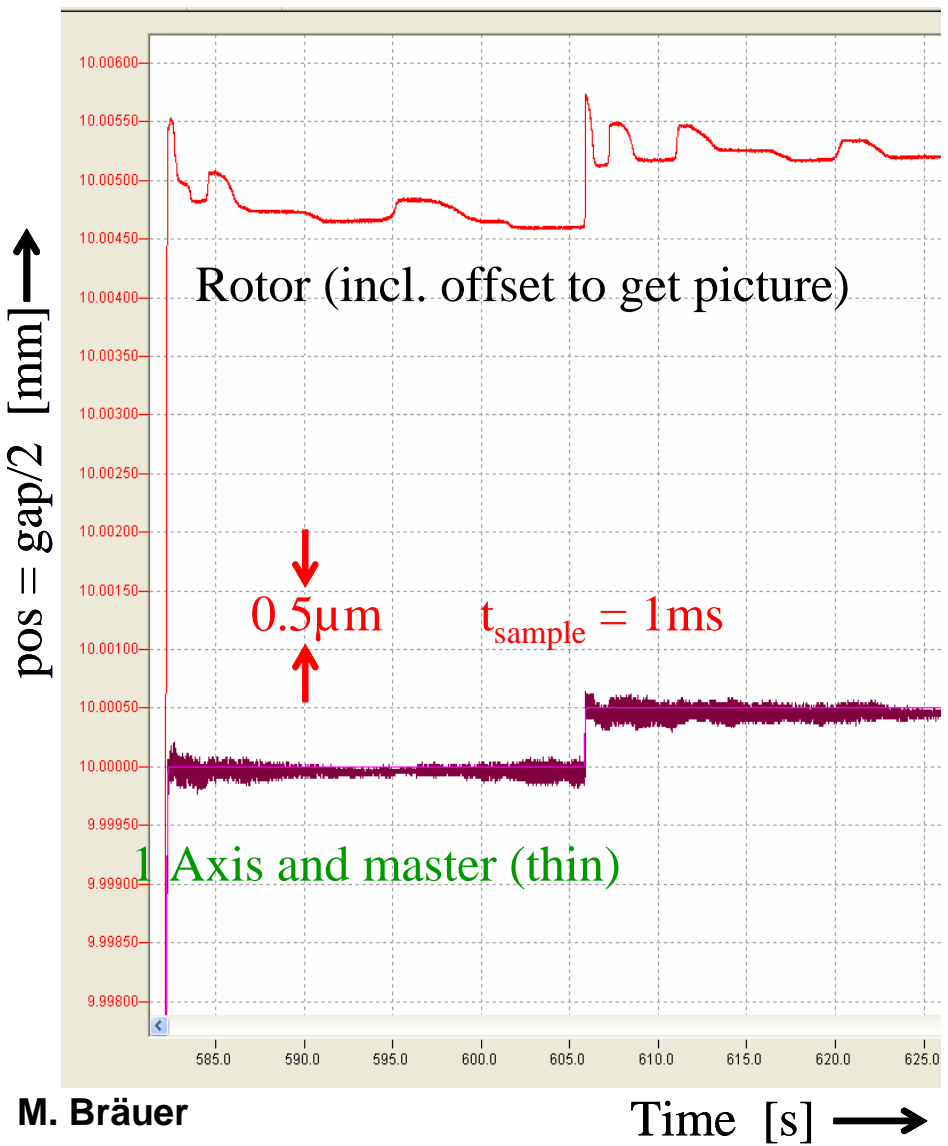


M. Bräuer

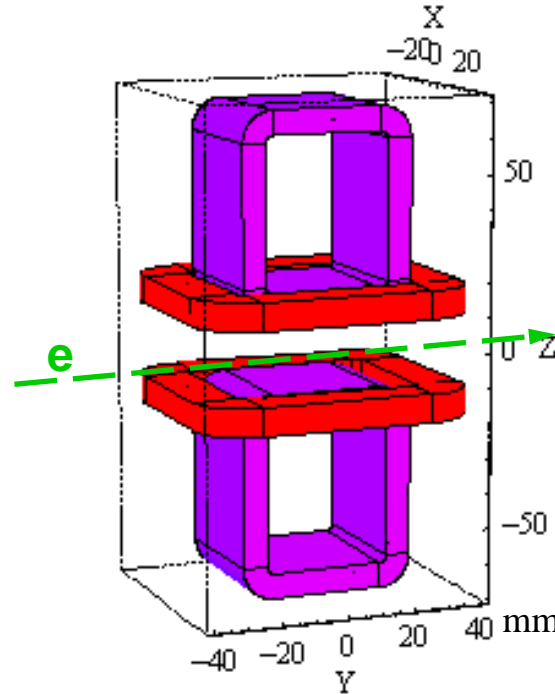




# Control System (2)



- active compensation of residual field integral (trajectory) changes
- air coils = hysteresis-free !
- very compact
- small adjustment range
- moderate field homogeneity
- integrated in ID control system
- first prototype completed  
→ 2 pairs used at VUV-FEL

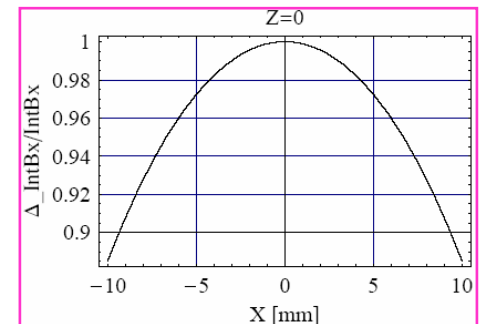


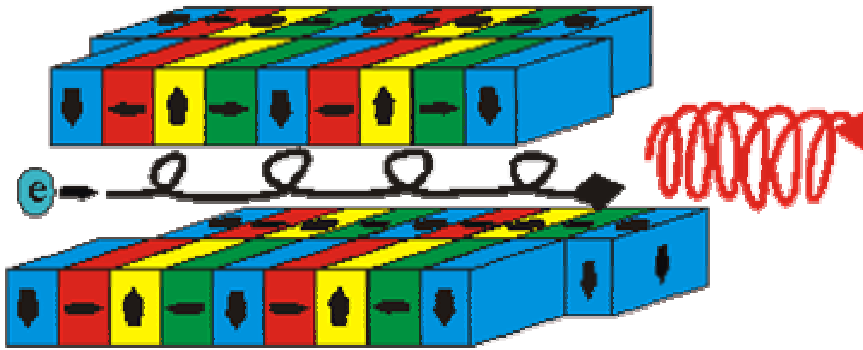
**horizontal steerer:  $B_z=4.2\text{mT}$ ,  $\text{Int}B_z=0.22\text{Tmm}$  (2.2Gm)**

**vertikal steerer:  $B_x=2.7\text{mT}$ ,  $\text{Int}B_x=0.22\text{Tmm}$  (2.2Gm)**

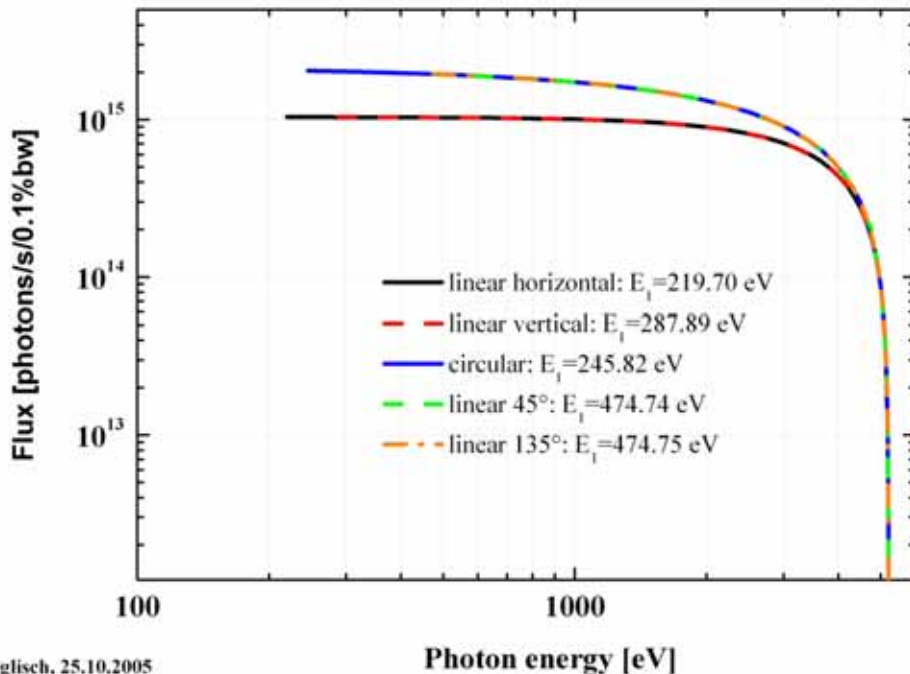
for  $j=2.03\text{A/mm}^2$  at 69% fill factor

...  $j \rightarrow 3 \text{ A/mm}^2$  might work



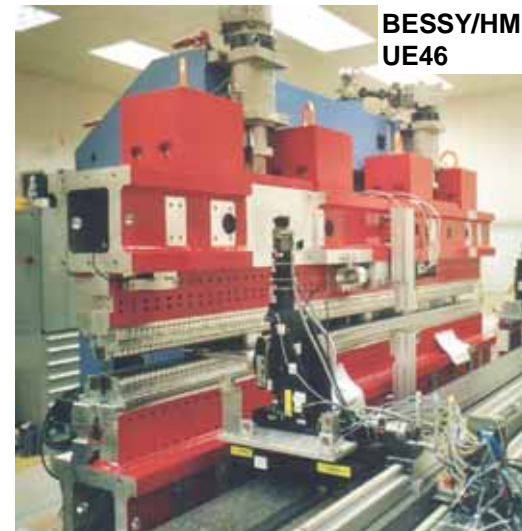


Flux in the central cone in the various operation types of the helical undulator



Operation mode	Shift[mm]	B <sub>eff</sub> [T]	K <sub>eff</sub>	E <sub>1</sub> [eV]
Hor. linear	00.0	1.10	6.7	220
Vert. linear	32.8	0.95	5.8	288
Circular	18.1	1.04	6.4	246
45 ° linear	17.3	0.73	4.5	475
135° linear	17.3	0.73	4.5	475

$\lambda_U = 65.6\text{mm}$ ,  $L = 5\text{m}$ ,  $\text{Gap} = 11\text{mm}$



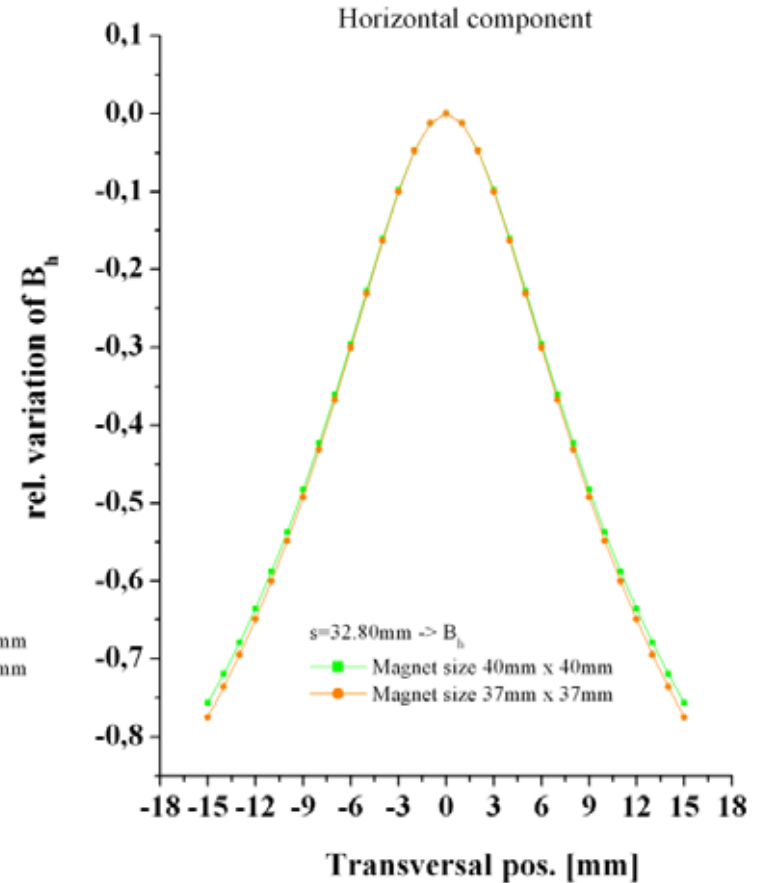
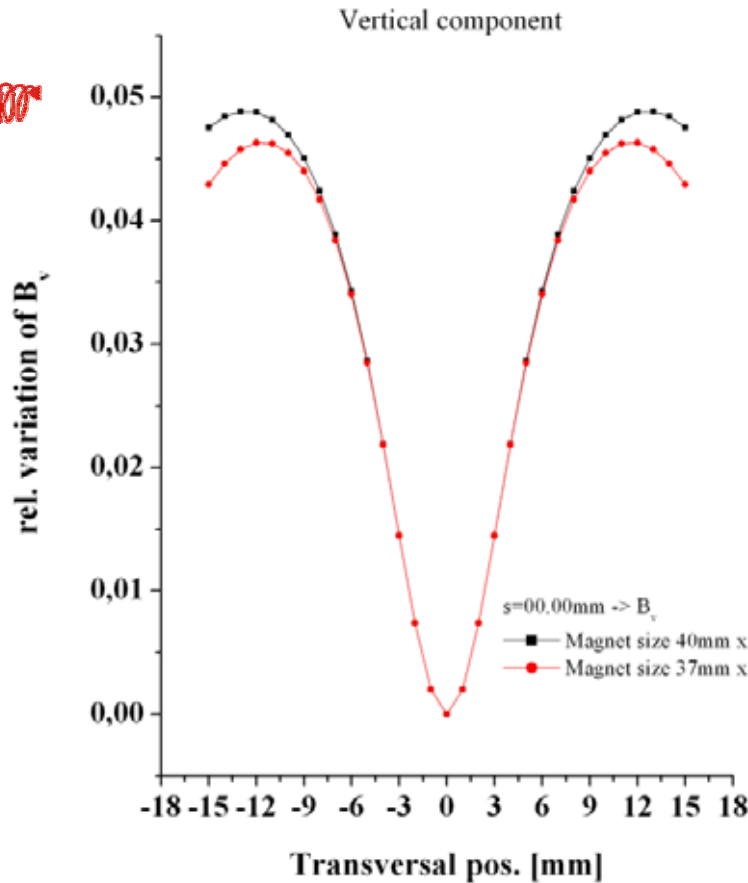
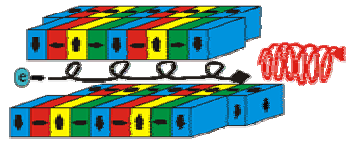
to be built in cooperation with BESSY

U. Englisch

... implications 1)

## Magnetic field components as a function of the transversal position

„field roll-off“



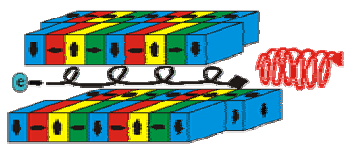
U. Englisch

→ decreases dynamic aperture, but can be handled (e.g. SLS, BESSY, ESRF ...)



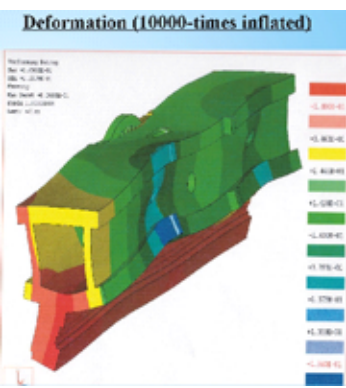
... implications 2)

## Forces acting on the lower girder of an UE with $\lambda_u = 65.6$ mm



■ antiparallel motion  
● parallel motion

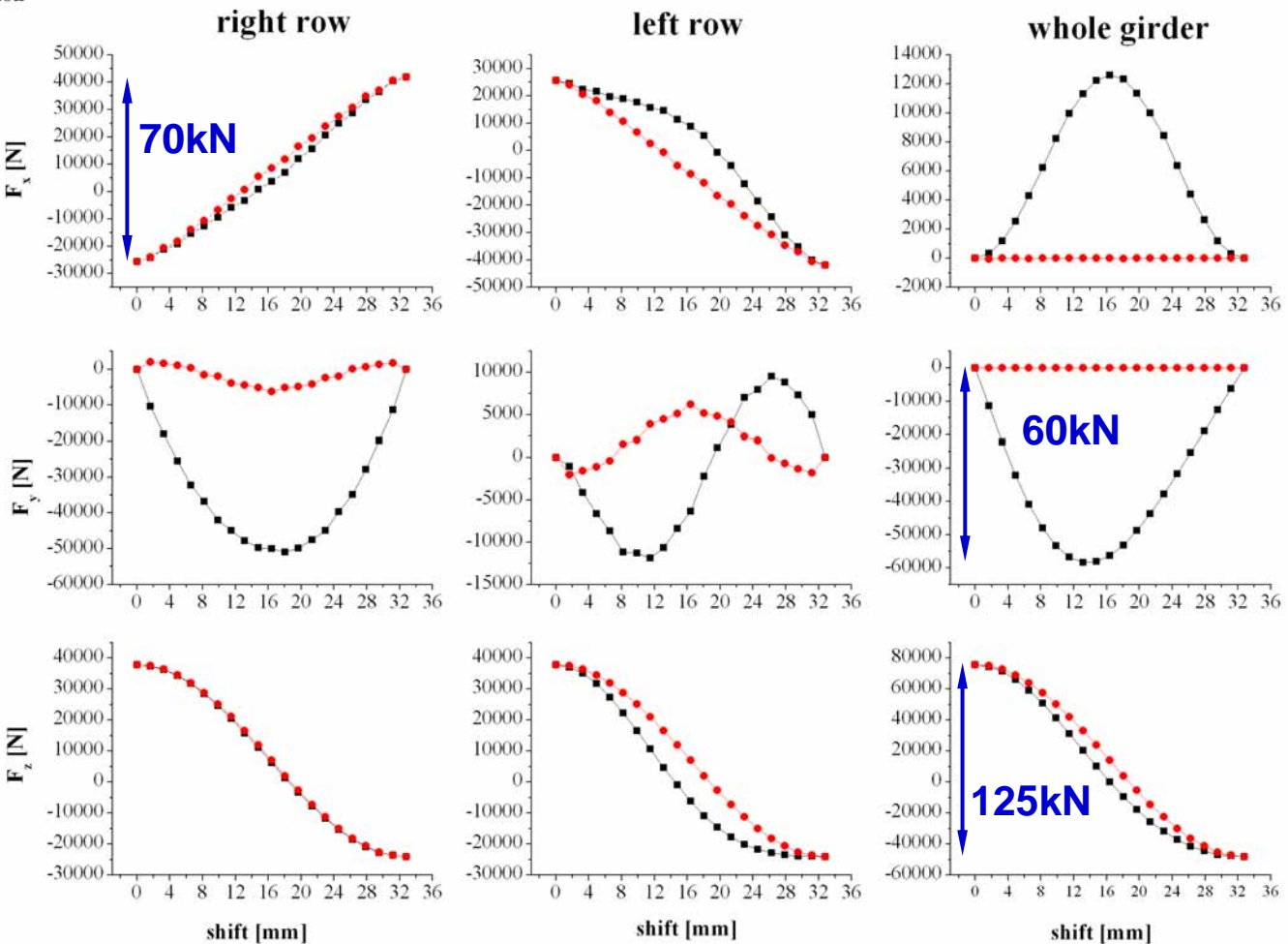
transversal force  $F_x$



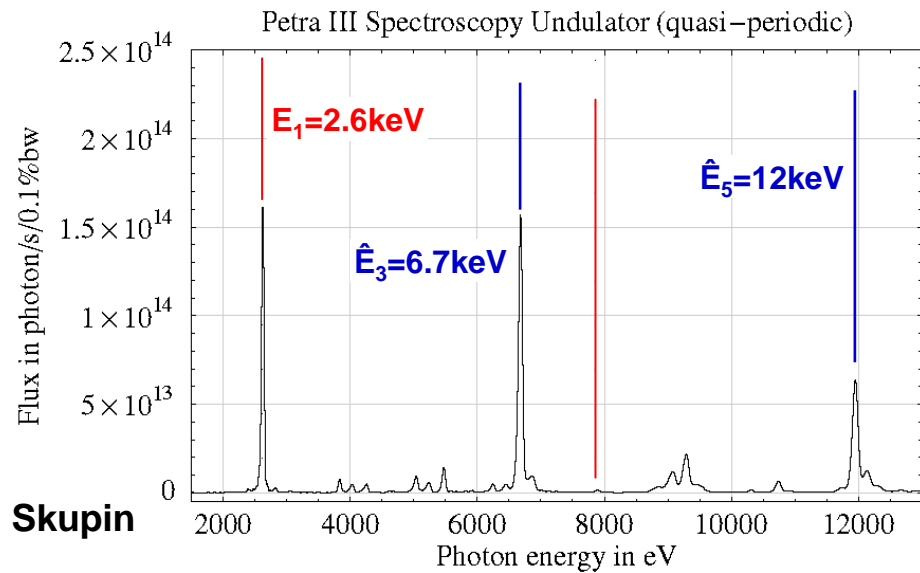
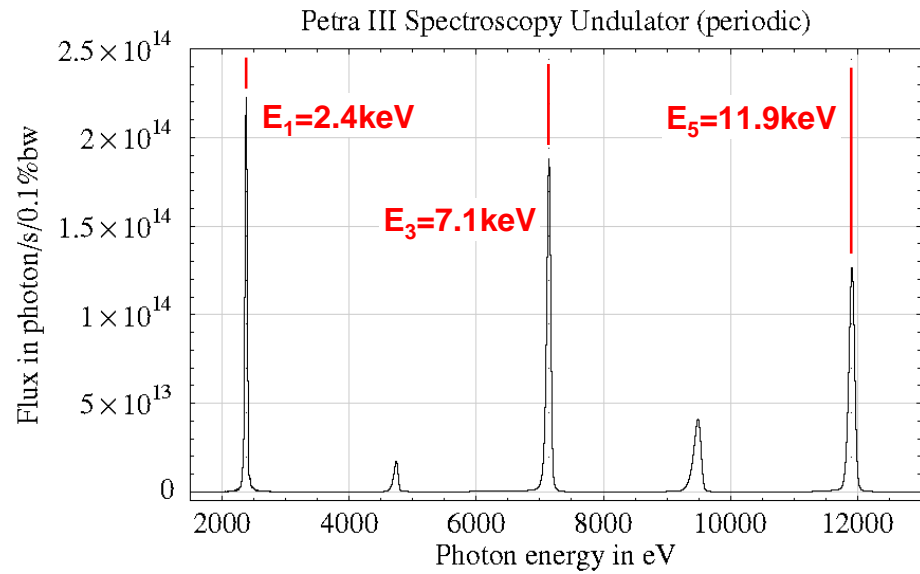
longitudinal force  $F_y$

U. Englisch

vertical force  $F_z$



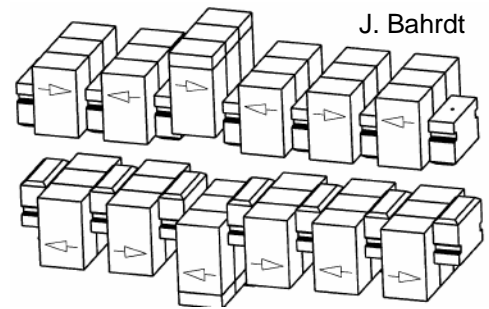
➔ needs modification of the gap mechanics to cope with the extra forces



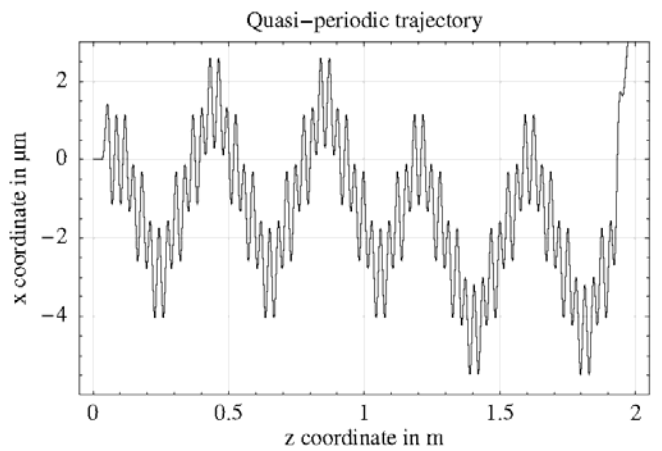
J. Skupin

Shift of the higher harmonics towards non-integer multiples

- Suppression of higher order radiation
- realized by modification of distinct magnets
- otherwise like the „Spectroscopy“-ID



$\lambda_U=31.4\text{mm}$ , gap=9.5mm, L=2m



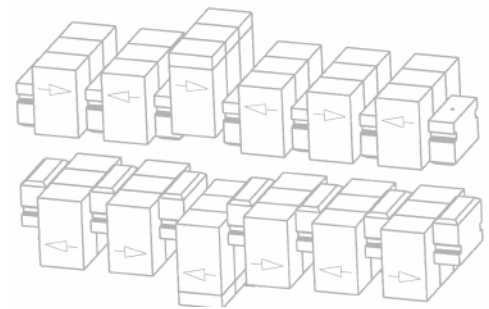


### Goals:

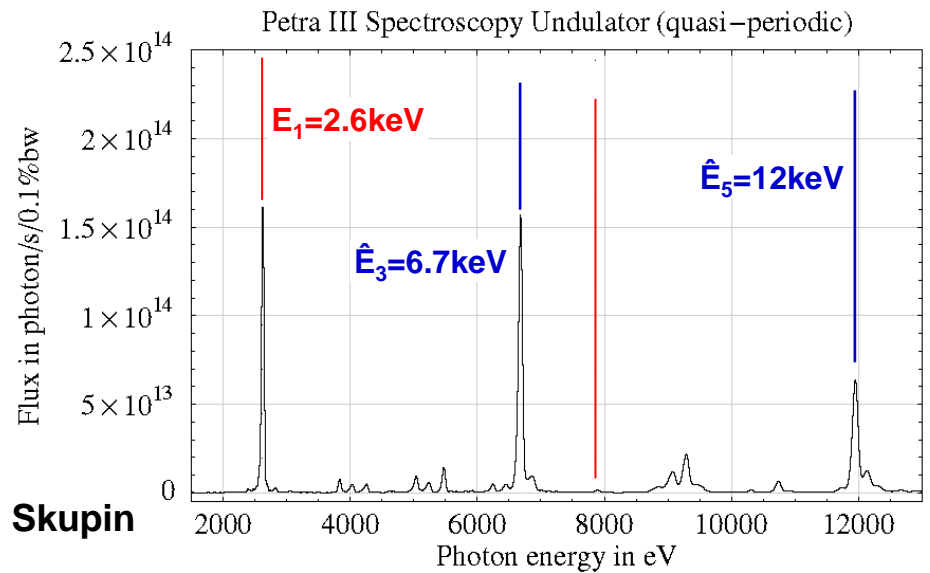
- Suppress 3rd order radiation
- Maximize intensity of shifted 3rd harmonic ( $E_3'$ )
- Suppress the 3rd harmonic of  $E_3'$

### Preliminary Results:

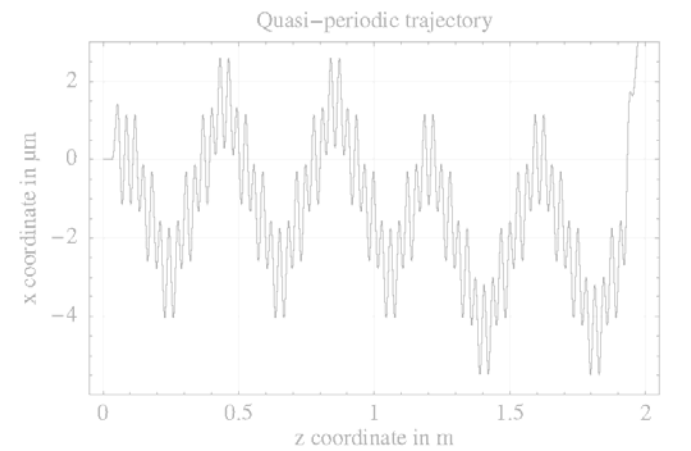
- 28% intensity reduction of 1st harmonic
- 99% reduction of 3rd harmonic contribution
- Slightly less suppression for the real device



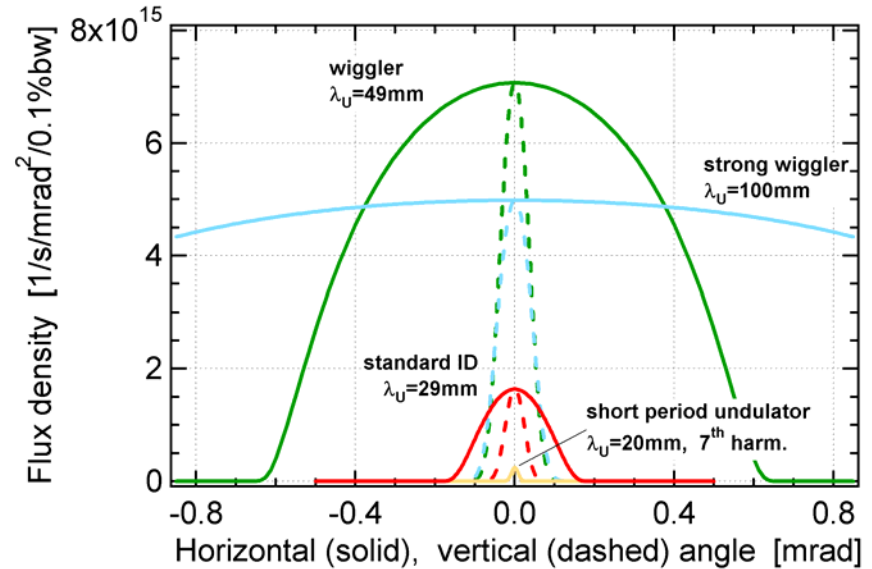
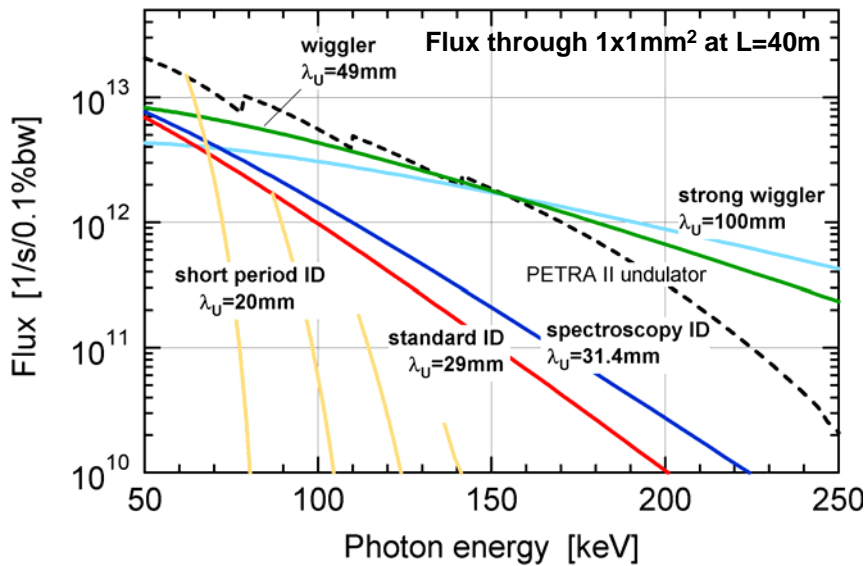
$\lambda_U=31.4\text{mm}$ , gap=9.5mm, L=2m



J. Skupin



Different options, still in discussion



## Alternative options

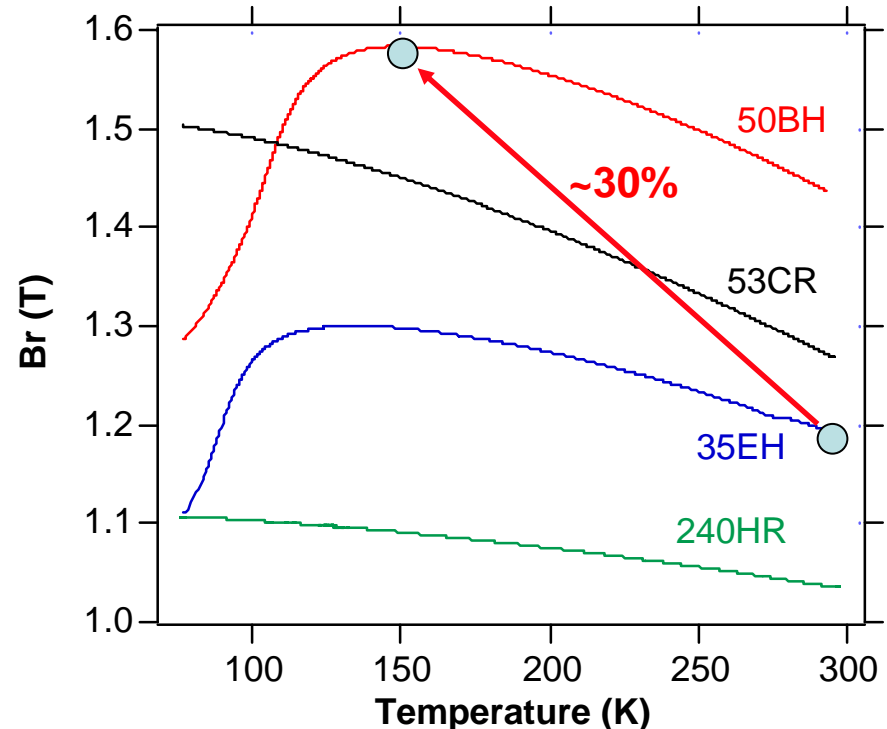
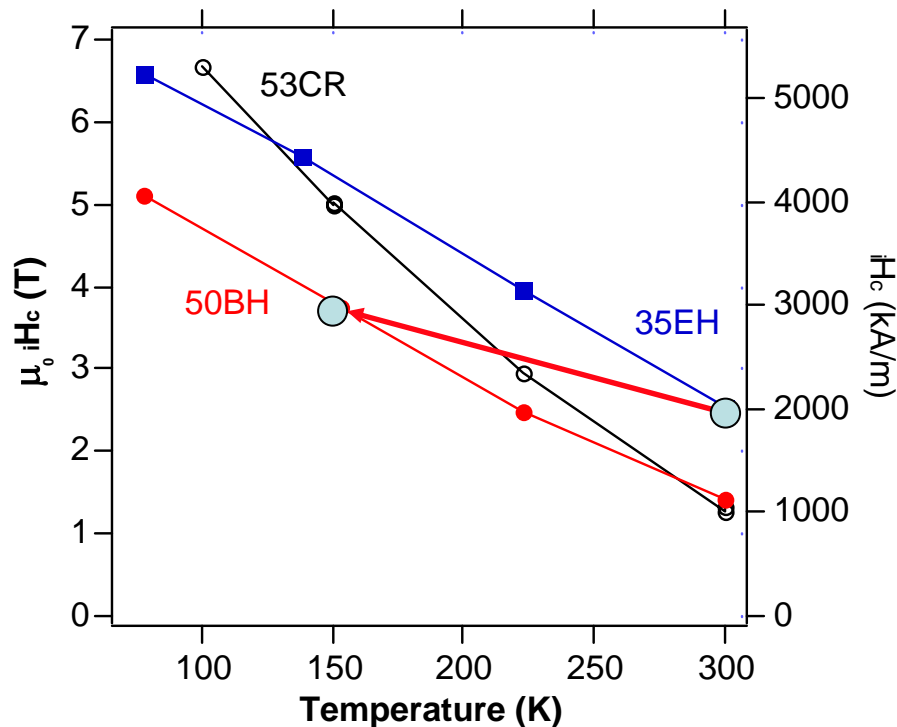
for small beam foci ( $30 \times 30 \mu\text{rad}^2$  or smaller): **Short period** undulators

- **In-vacuum** undulator (300K) : beneficial for small beam foci at high energies!
- **Cryo-In-vacuum** undulator (T=150K) : present developments at various places promising!
- **Superconducting** undulator (T=4K) : best once technologically established

T. Hara, SPring-8, WUS2005,  
PRST-AB 7 (2004)

## Concept of cryogenic insertion devices

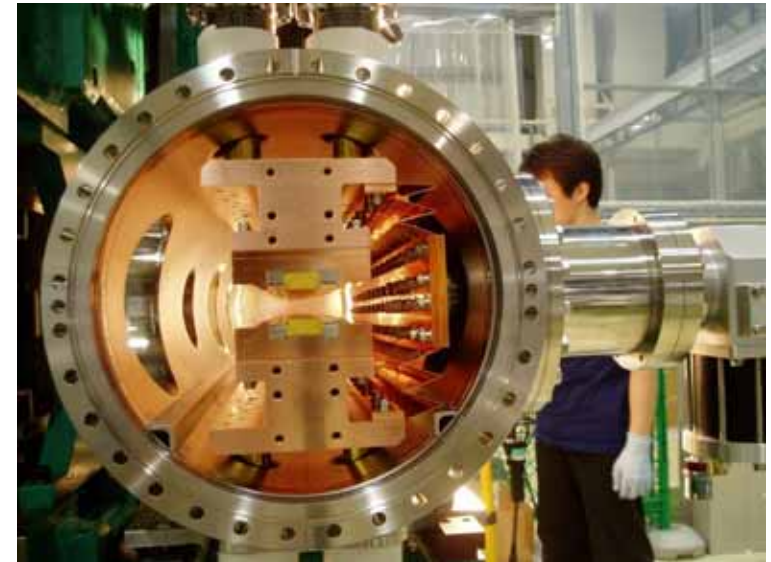
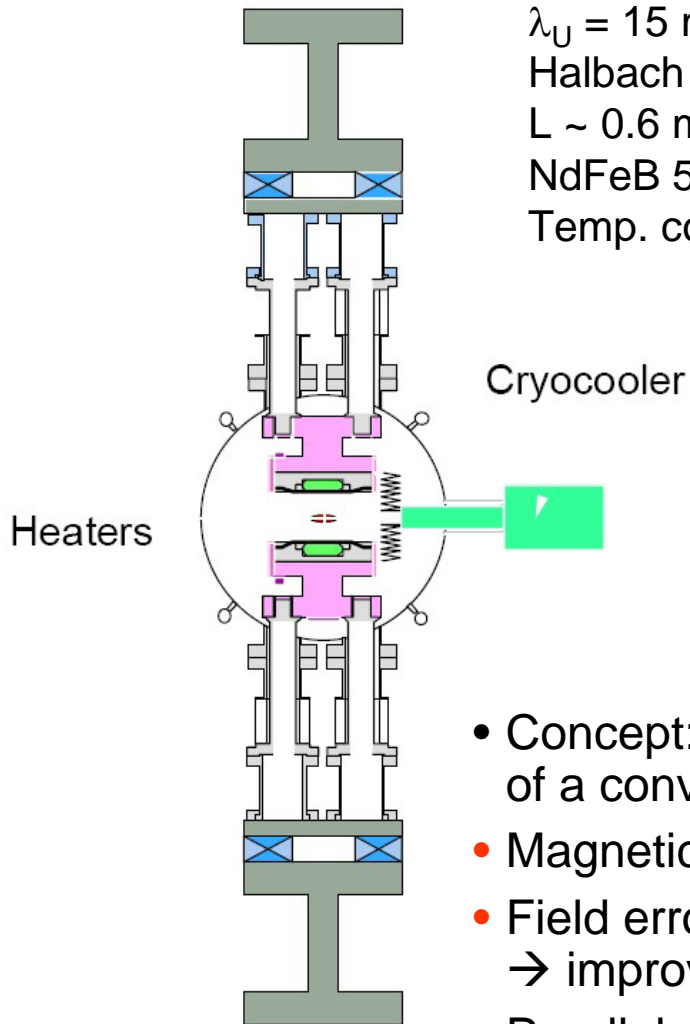
- Increased coercivity at cryogenic temperatures ( $> 77\text{K}$ )  
=> choice of high  $B_r$  material, high resistance against demagnetization.
- Increased remanent field ( $B_r$ )



T. Hara, SPring-8, WUS2005,  
PRST-AB 7 (2004)

## Prototype

$\lambda_U = 15$  mm  
Halbach ppm  
 $L \sim 0.6$  m  
NdFeB 50BH  
Temp. controlled by heaters



- Concept: Adding a cryocooler and modifying support shafts of a conventional in-vacuum undulator.
- Magnetic properties according expectations
- Field errors due to thermal deformation  
→ improve mechanics & isolation
- Parallel developments at ESRF and NSLS



# Cryo-In-Vacuum ID for hard X-rays



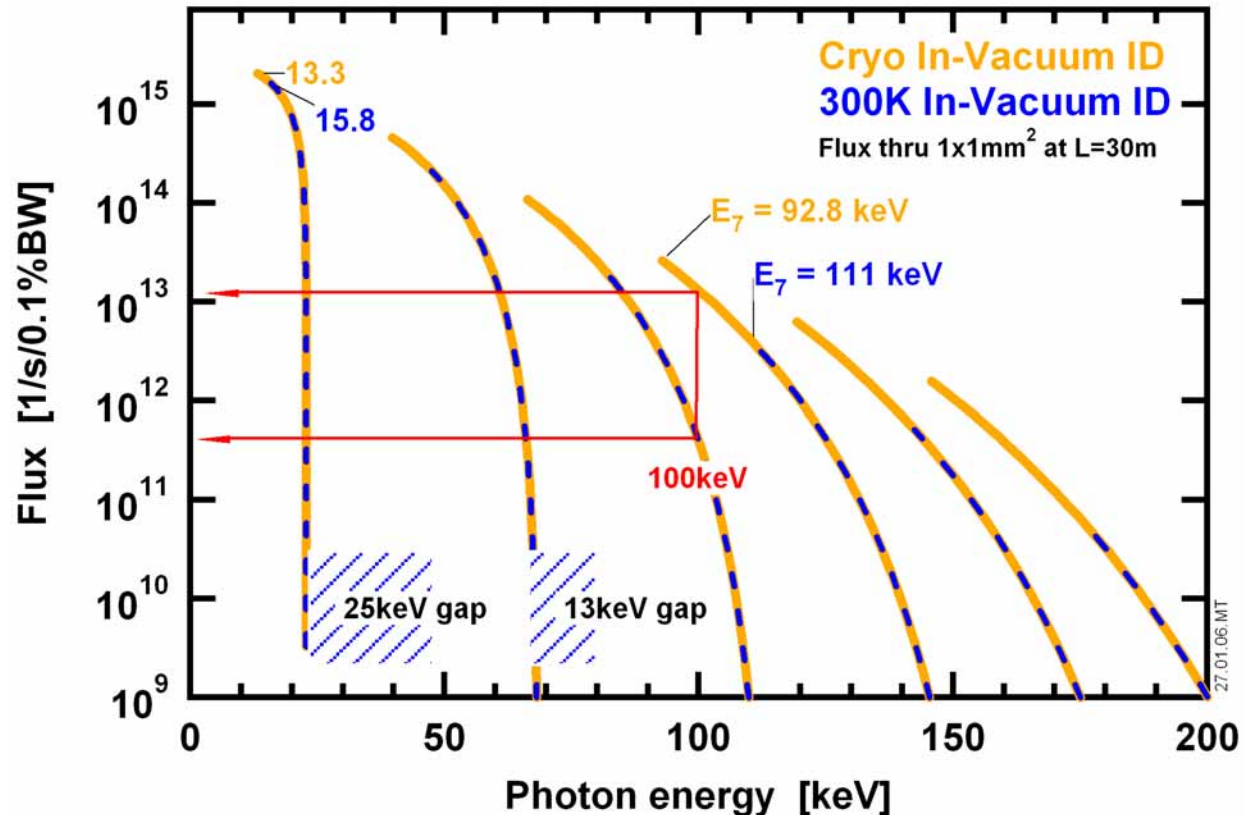
for PETRA III: parameters ~like SPring8

gap = 5.5mm      NdFeB 50BH  
 $\lambda_U = 15\text{mm}$        $T = 150\text{K}$   
 $L = 4\text{m}$        $M_r \sim 1.55\text{T}$   
 $B_0 = 0.86\text{T}$   
 $K = 1.2$   
 $E_1 = 13.3\text{ keV}$

for comparison:

**In-Vacuum ID,  $T=300\text{K}$**

gap = 5.5mm  
 $\lambda_U = 15\text{mm}$   
 $L = 4\text{m}$   
 $B_0 = 0.67\text{T}$   
 $K = 0.93$   
 $E_1 = 15.8\text{ keV}$





# Cryo-In-Vacuum ID for hard X-rays



**for PETRA III:** parameters ~like SPring8

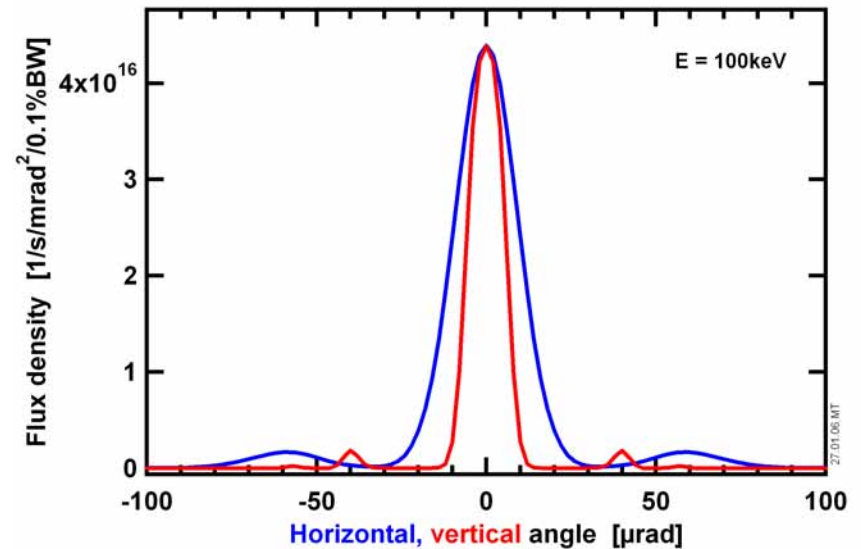
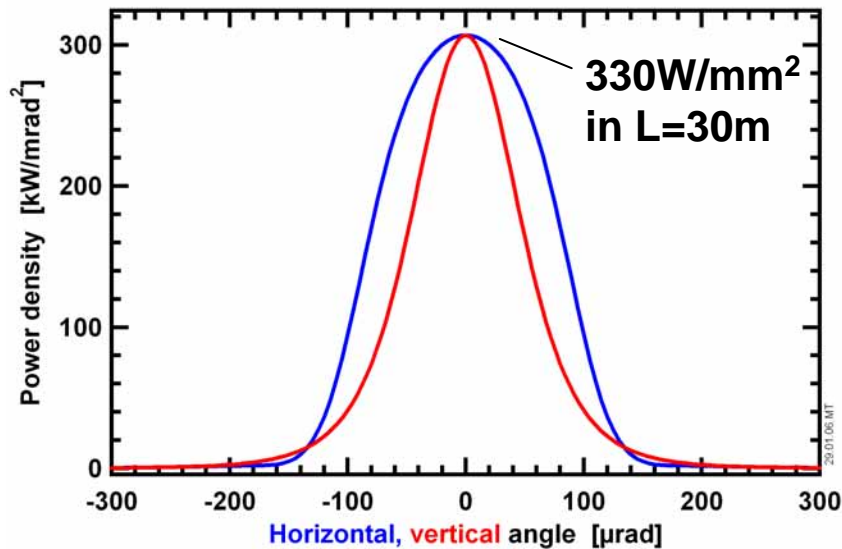
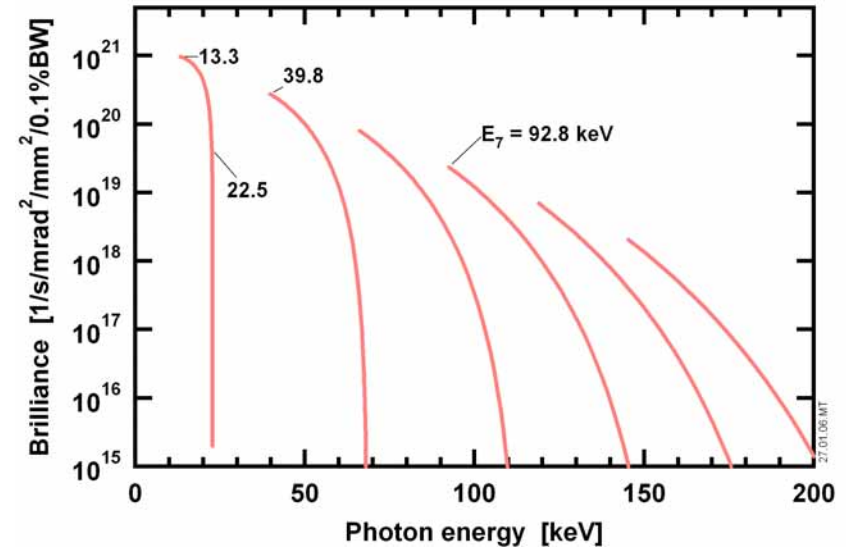
gap = 5.5mm      NdFeB 50BH

$\lambda_U = 15\text{mm}$       **T = 150K**

L = 4m

$B_0 = 0.86\text{T}$       K = 1.2

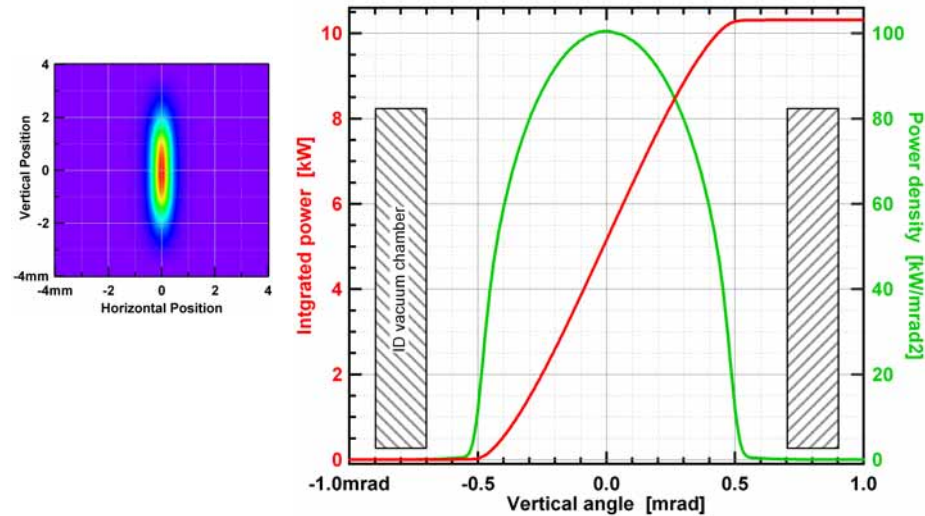
$P_{\text{tot}} = 6.7\text{kW}$





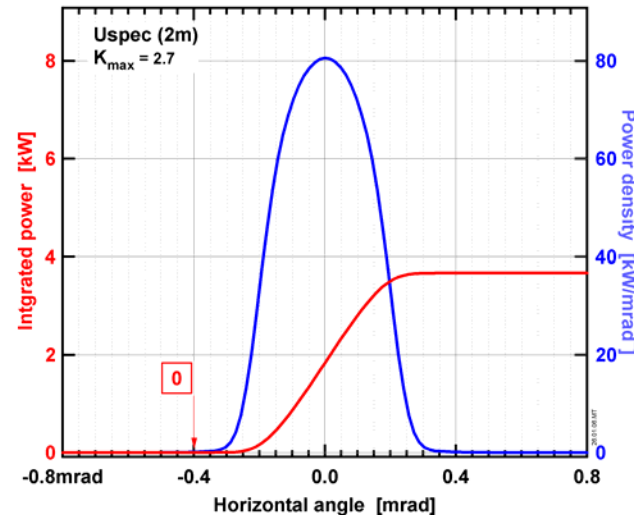
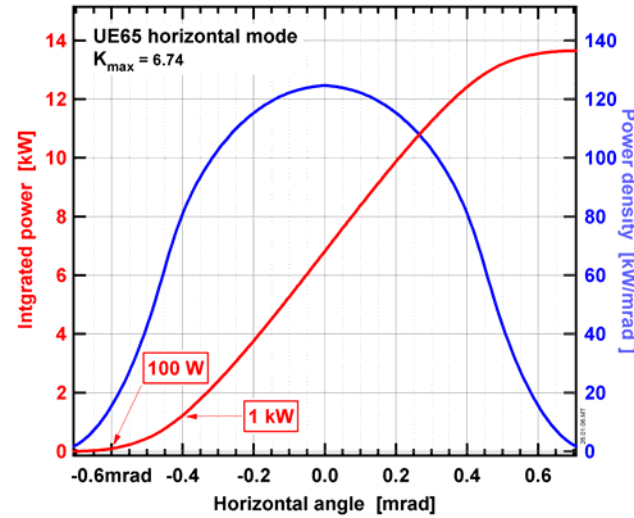
... implications:

## APPLE2: Linear vertical mode



- requires large vertical aperture in ID chamber and front end until 1st absorber
- chamber cooling if necessary (Bessy)

## 5m long straights:



## 2m canted straights





Thanks